

## **EXHAUST GAS PURIFYING DEVICE FOR ENGINE**

### **BACKGROUND OF THE INVENTION**

**[0001]** The present invention relates to an exhaust gas purifying device for an engine, and, more specifically, to an exhaust gas purifying device for an engine to remove NOx from exhaust gas of the engine.

**[0002]** An exhaust gas purifying device for an engine that performs a lean burn operation is known. Such a device is equipped with a NOx trap catalyst including a NOx trap material to absorb NOx during a state of high oxygen concentration in the exhaust gas and release the absorbed NOx during a state of low oxygen concentration in the exhaust gas. The NOx absorption capacity of the NOx trap material is limited. Accordingly, in this exhaust gas purifying device, when the amount of NOx absorbed in the NOx trap material reaches a saturation amount, a purifying control (so called, rich-spike control) is performed which changes an engine operating condition from the lean burn operation to an operation with a stoichiometric air-fuel ratio or the like to lower the concentration of oxygen in the exhaust gas. This control causes the NOx trap material to release NOx absorbed and to reduce and thereby purify the released NOx with a catalytic metal included in the NOx trap catalyst.

**[0003]** As a device for conducting a diagnosis of deterioration for this kind of NOx trap catalyst, Japanese Patent Laid-Open Publication No. 2000-337131 proposes a device making use of a peak value of an output of the NOx sensor during the rich-spike control. In this device, the deterioration is determined such that the lower the peak value of the NOx sensor at a transitional stage to a rich side becomes, the more NOx trap capacity of the NOx trap material has reduced, that is, the NOx trap catalyst has deteriorated.

**[0004]** The NOx trap catalyst, in general, includes a catalytic metal (noble metal) for oxidizing NOx and an O<sub>2</sub> storage material for absorbing oxygen. However, the deterioration diagnosis device described in the above patent publication may not diagnose

the deterioration of the reduction capacity of the catalytic metals or deterioration of O<sub>2</sub> storage capacity of the O<sub>2</sub> storage material.

[0005] Further, when the rich-spike control is executed, the following reactions occur sequentially: O<sub>2</sub> release from the O<sub>2</sub> storage material; oxidization of an exhaust gas composition by the released O<sub>2</sub>; NO<sub>x</sub> release from the NO<sub>x</sub> trap material; and reduction of the released NO<sub>x</sub> by the catalytic metal. However, if the air-fuel ratio of the exhaust gas is changed rapidly toward a rich side during NO<sub>x</sub> release, as performed in the deterioration diagnosis device described in the above publication, results of some reactions described above adversely affect or are mixed up with the output value of the NO<sub>x</sub> sensor due to an output delay of the NO<sub>x</sub> sensor or the like. Accordingly, a state of these reactions is not detected appropriately, so that each of deteriorations of O<sub>2</sub> storage capacity of the O<sub>2</sub> storage material (deterioration of O<sub>2</sub> storage material) and reduction capacity of the catalytic metal (deterioration of catalytic metal) can not be diagnosed accurately.

#### SUMMARY OF THE INVENTION

[0006] The present invention has been devised in view of the above-described problems, and an object of the present invention is to provide an exhaust gas purifying device for an engine that performs the diagnosis function of diagnosing accurately each of deterioration of O<sub>2</sub> storage capacity of an O<sub>2</sub> storage material and NO<sub>x</sub> reduction capacity of a catalytic metal, which are included in a NO<sub>x</sub> trap catalyst.

[0007] In order to achieve the above-described object, the first aspect of the present invention provides an exhaust gas purifying device for an engine, comprising a NO<sub>x</sub> trap catalyst disposed in an exhaust gas passage of the engine including a NO<sub>x</sub> trap material to absorb NO<sub>x</sub> while oxygen of an exhaust gas is in high concentration and release the absorbed NO<sub>x</sub> while oxygen is in low concentration, a catalytic metal to purify the NO<sub>x</sub> released from the NO<sub>x</sub> trap material, and an O<sub>2</sub> storage material to absorb O<sub>2</sub> while oxygen

of the exhaust gas is in high concentration and release the absorbed O<sub>2</sub> while oxygen is in low concentration, a NO<sub>x</sub> sensor disposed in the exhaust gas passage downstream of the NO<sub>x</sub> trap catalyst, NO<sub>x</sub> absorbed amount calculating section for calculating the amount of NO<sub>x</sub> absorbed in the NO<sub>x</sub> trap catalyst, NO<sub>x</sub> release controlling section for lowering the concentration of oxygen of the exhaust gas in the exhaust gas passage so as to cause the NO<sub>x</sub> trap catalyst to release NO<sub>x</sub> absorbed when the amount of the NO<sub>x</sub> absorbed in the NO<sub>x</sub> trap catalyst reaches a specified amount, operating condition detecting section for detecting an operating condition of the engine, determination section for determining whether a specified diagnosis condition to diagnose the NO<sub>x</sub> trap catalyst is satisfied or not, according to the engine operating condition detected by the operating condition detecting section, detecting section for detecting whether or not O<sub>2</sub> release from the O<sub>2</sub> storage material caused by oxygen concentration lowering of the exhaust gas in the exhaust gas passage by the NO<sub>x</sub> release controlling section has terminated, diagnosing section for diagnosing a degree of deterioration of respective capacities of the O<sub>2</sub> storage material and the catalytic metal that are included in the NO<sub>x</sub> trap catalyst when the specified diagnosis condition is satisfied, the diagnosing section diagnosing a degree of deterioration of O<sub>2</sub> storage capacity of the O<sub>2</sub> storage material according to output values of the NO<sub>x</sub> sensor that are generated during a term from the beginning of the oxygen concentration lowering of the NO<sub>x</sub> release controlling section until a termination of the O<sub>2</sub> release from the O<sub>2</sub> storage material, the diagnosing section diagnosing a degree of deterioration of NO<sub>x</sub> reduction capacity of the catalytic metal according to an output value of the NO<sub>x</sub> sensor that is generated after the termination of the O<sub>2</sub> release from the O<sub>2</sub> storage material, wherein the NO<sub>x</sub> release controlling section is configured such that a speed of lowering oxygen concentration thereby when the specified diagnosis condition is satisfied is slower than that when the specified diagnosis condition is not satisfied.

[0008] According to the exhaust gas purifying device for an engine of the first aspect of the invention, each of deterioration of O<sub>2</sub> storage capacity of the O<sub>2</sub> storage material and

NOx reduction capacity of the catalytic metal, which are included in the NOx trap catalyst, can be diagnosed accurately, during a control (rich-spike control) for NOx release from the NOx trap catalyst for lowering the concentration of oxygen of the exhaust gas in the exhaust gas passage.

[0009] The second aspect of the present invention provides the exhaust gas purifying device of an engine of the first aspect of the invention, wherein the detecting section comprise an O2 sensor disposed in the exhaust gas passage downstream of the NOx trap catalyst, and O2 release termination determining section for determining that the O2 release from the O2 storage material has terminated when an output value of the O2 sensor indicates a value equivalent to a stoichiometric air-fuel ratio of the exhaust gas.

[0010] The third aspect of the present invention provides the exhaust gas purifying device of an engine of the first aspect of the invention, wherein the diagnosing section is configured so as to diagnose that O2 storage capacity of the O2 storage material included in the NOx trap catalyst has deteriorated when an integrated value of output values of the NOx sensor with respect to time during a term from the beginning of the oxygen concentration lowering of the NOx release controlling section until a termination of the O2 release from the O2 storage material is smaller than a first threshold value.

[0011] The fourth aspect of the present invention provides the exhaust gas purifying device of an engine of the first aspect of the invention, wherein the diagnosing section is configured so as to diagnose that O2 storage capacity of the O2 storage material included in the NOx trap catalyst has deteriorated when a value that is gained by dividing a difference between a maximum value and a minimum value of output values of the NOx sensor that are generated during a term from the beginning of the oxygen concentration lowering of the NOx release controlling section until a termination of the O2 release from the O2 storage material, by the time spent during the term is greater than a second threshold value.

[0012] According to the exhaust gas purifying device for an engine of the third and fourth aspects of the invention, the deterioration of O2 storage capacity of the O2 storage material

included in the NOx trap catalyst can be detected by making use of the output values of the NOx sensor that are generated during the term from the beginning of rich-spike control by the NOx release controlling section until the termination of the O2 release from the O2 storage material.

[0013] The fifth aspect of the present invention provides the exhaust gas purifying device of an engine of the third aspect of the invention, further comprising first correcting section for correcting the first threshold value, in such a way that the greater a difference between the amount of absorbed NOx calculated by the NOx absorbed amount calculating section and the specified amount is, the greater value the first threshold value for diagnosing the deterioration of O2 storage capacity of the O2 storage material included in the NOx trap catalyst is corrected to.

[0014] The sixth aspect of the present invention provides the exhaust gas purifying device of an engine of the fourth aspect of the invention, further comprising second correcting section for correcting the second threshold value, in such a way that the greater a difference between the amount of absorbed NOx calculated by the NOx absorbed amount calculating section and the specified amount is, the smaller value the second threshold value for diagnosing the deterioration of O2 storage capacity of the O2 storage material included in the NOx trap catalyst is corrected to.

[0015] When the extremely larger amount of NOx than the specified amount has been absorbed for some reason, such as under a situation that the engine has been shut down during the previous rich-spike control, executing the deterioration diagnosis of the O2 storage material by using a normal threshold value may provide an erroneous diagnosis that the O2 storage material has not deteriorated yet, in spite of the fact that it has already deteriorated, because of too much NOx absorbed in the NOx trap catalyst. According to the exhaust gas purifying device for an engine of these aspects of the invention, however, when it is determined that the amount of NOx absorbed in the NOx trap catalyst is greater than the specified amount for determining the beginning of rich-spike control, the threshold

value for determining the deterioration of O<sub>2</sub> storage capacity is corrected in such a manner that determination of the deterioration of O<sub>2</sub> storage capacity becomes apt to occur, according to the difference between the NO<sub>x</sub> absorbed amount and the specified amount for the determination. Accordingly, the above-described erroneous diagnosis can be prevented.

[0016] The seventh aspect of the present invention provides the exhaust gas purifying device of an engine of the first aspect of the invention, wherein the diagnosing section is configured so as to diagnose that NO<sub>x</sub> reduction capacity of the catalytic metal included in the NO<sub>x</sub> trap catalyst has deteriorated when a maximum value of output values of the NO<sub>x</sub> sensor that are generated after a termination of the O<sub>2</sub> release from the O<sub>2</sub> storage material is greater than a third threshold value.

[0017] The eighth aspect of the present invention provides the exhaust gas purifying device of an engine of the first aspect of the invention, wherein the diagnosing section is configured so as to diagnose that NO<sub>x</sub> reduction capacity of the catalytic metal included in the NO<sub>x</sub> trap catalyst has deteriorated when an integrated value of output values of the NO<sub>x</sub> sensor with respect to time during a term from a termination of the O<sub>2</sub> release from the O<sub>2</sub> storage material until a specified time has passed since the termination of the O<sub>2</sub> release is greater than a fourth threshold value.

[0018] The ninth aspect of the present invention provides the exhaust gas purifying device of an engine of the first aspect of the invention, wherein the diagnosing section is configured so as to diagnose that NO<sub>x</sub> reduction capacity of the catalytic metal included in the NO<sub>x</sub> trap catalyst has deteriorated when a value that is gained by dividing a difference between a maximum value output values of the NO<sub>x</sub> sensor that are generated during a term from a termination of the O<sub>2</sub> release from the O<sub>2</sub> storage material until a specified time has passed since the termination of the O<sub>2</sub> release and an output value of the NO<sub>x</sub> sensor that is generated at the time when the O<sub>2</sub> release from the O<sub>2</sub> storage material has terminated, by a difference between the output value of the NO<sub>x</sub> sensor that is generated at the time when the

O<sub>2</sub> release from the O<sub>2</sub> storage material has terminated and an output value of the NO<sub>x</sub> sensor that is generated at the time when the specified time has passed is greater than a fifth threshold value.

[0019] According to the exhaust gas purifying device for an engine of the seventh through ninth aspects of the invention, the deterioration of NO<sub>x</sub> reduction capacity of the catalytic metal included in the NO<sub>x</sub> trap catalyst can be detected by making use of the output values of the NO<sub>x</sub> sensor that are generated during a specified term after the termination of the O<sub>2</sub> release from the O<sub>2</sub> storage material.

[0020] The tenth aspect of the present invention provides the exhaust gas purifying device of an engine of the eighth aspect of the invention, wherein the diagnosing section further comprising second correcting section for correcting the fourth threshold value, in such a way that the greater a difference between the amount of absorbed NO<sub>x</sub> calculated by the NO<sub>x</sub> absorbed amount calculating section and the specified amount is, the greater value the fourth threshold value is corrected to.

[0021] When the extremely larger amount of NO<sub>x</sub> than the specified amount has been absorbed for some reason, such as under a situation that the engine has been shut down during the previous rich-spike control, executing the deterioration diagnosis of the catalytic metal by using a normal threshold value may provide an erroneous diagnosis that the catalytic metal has not deteriorated yet, in spite of the fact that it has already deteriorated, because of too much NO<sub>x</sub> absorbed in the NO<sub>x</sub> trap catalyst. According to the exhaust gas purifying device for an engine of the tenth aspect of the invention, however, when it is determined that the amount of NO<sub>x</sub> absorbed in the NO<sub>x</sub> trap catalyst is greater than the specified amount for determining the beginning of rich-spike control, the threshold value for determining the deterioration of catalytic metal capacity is corrected in such a manner that determination of the deterioration of catalytic metal capacity becomes unlikely to occur, according to the difference between the NO<sub>x</sub> absorbed amount and the specified amount for the determination. Accordingly, the above-described erroneous diagnosis can be

prevented.

[0022] The eleventh aspect of the present invention provides the exhaust gas purifying device of an engine of the first aspect of the invention, further comprising NOx trap capacity diagnosing section for diagnosing that NOx trap capacity of the NOx trap material included in the NOx trap catalyst has deteriorated when the sum of an integrated value of output values of the NOx sensor with respect to time during a term from the beginning of the oxygen concentration lowering of the NOx release controlling section until a termination of the O<sub>2</sub> release from the O<sub>2</sub> storage material and an integrated value of output values of the NOx sensor with respect to time during a term from the termination of the O<sub>2</sub> release from the O<sub>2</sub> storage material until a specified time has passed since the termination of the O<sub>2</sub> release is smaller than a sixth threshold value.

[0023] The twelfth aspect of the present invention provides the exhaust gas purifying device of an engine of the first aspect of the invention, further comprising specified-amount correcting section for correcting the specified amount of NOx absorbed amount that is used by the NOx release controlling section in executing the NOx release to a smaller value when it is diagnosed that NOx reduction capacity of the catalytic metal included in the NOx trap catalyst has deteriorated.

[0024] According to the exhaust gas purifying device for an engine of the twelfth aspect of the invention, when NOx reduction capacity of the catalytic metal included in the NOx trap catalyst has deteriorated, that is, when the amount of NOx which can be reduced by the catalytic metal, the rich-spike control is performed in the condition where the amount of NOx absorbed in the NOx trap catalyst is small. Accordingly, this can decrease the amount of NOx released during the rich-spike control and the amount of NOx to be reduced by the catalytic metal, resulting in lightening NOx reduction capacity required in the catalytic metal.

[0025] The thirteenth aspect of the present invention provides the exhaust gas purifying device of an engine of the first aspect of the invention, further comprising oxygen

concentration correcting section for setting the concentration of oxygen of the exhaust gas in the exhaust gas passage, which is lowered by the NOx release controlling section, to a higher value when it is diagnosed that O<sub>2</sub> storage capacity of the O<sub>2</sub> storage material included in the NOx trap catalyst has deteriorated.

[0026] The concentration of oxygen of the exhaust gas in the exhaust gas passage during the rich-spike control is set to a low value in expectation of O<sub>2</sub> release from the O<sub>2</sub> storage material. Accordingly, if O<sub>2</sub> storage capacity of the O<sub>2</sub> storage material has been decreased, an expected amount of O<sub>2</sub> may not be released, resulting in a state of oxygen deficit. Herein, according to the exhaust gas purifying device for an engine of the thirteenth aspect of the invention, when O<sub>2</sub> release capacity of the O<sub>2</sub> storage material included in the NOx trap catalyst has deteriorated, that is, when the mount of O<sub>2</sub> released from the O<sub>2</sub> storage material during the rich-spike control decreases, for example, the oxygen concentration of the exhaust gas in the exhaust gas passage during the rich-spike control is set to a high value by an air-fuel control or the like. Accordingly, the shortage of O<sub>2</sub> released from the O<sub>2</sub> storage material can be compensated.

[0027] The fourteenth aspect of the present invention provides the exhaust gas purifying device of an engine of the first aspect of the invention, further comprising second diagnosing section for diagnosing that O<sub>2</sub> storage capacity of the O<sub>2</sub> storage material has deteriorated when the time spent from the beginning of the oxygen concentration lowering of the NOx release controlling section until a termination of the O<sub>2</sub> release from the O<sub>2</sub> storage material is shorter than a specified time.

[0028] According to the exhaust gas purifying device for an engine of the fourteenth aspect of the invention, the diagnosis of deterioration of the O<sub>2</sub> storage material is executed based on only the time of O<sub>2</sub> release from the O<sub>2</sub> storage material.

[0029] The fifteenth aspect of the present invention provides the exhaust gas purifying device of an engine of the fourteenth aspect of the invention, wherein the second diagnosing section further comprising third correcting section for correcting the specified time to be

used for diagnosing O<sub>2</sub> storage capacity of the NO<sub>x</sub> trap catalyst, in such a way that the greater a difference between the amount of absorbed NO<sub>x</sub> calculated by the NO<sub>x</sub> absorbed amount calculating section and the specified amount is, the longer value the specified time is corrected to.

[0030] The sixteenth aspect of the present invention provides an exhaust gas purifying device of an engine, comprising, a NO<sub>x</sub> trap catalyst disposed in an exhaust gas passage of the engine including a NO<sub>x</sub> trap material to absorb NO<sub>x</sub> while oxygen of an exhaust gas is in high concentration and release the absorbed NO<sub>x</sub> while oxygen is in low concentration, a catalytic metal to purify the NO<sub>x</sub> released from the NO<sub>x</sub> trap material, and an O<sub>2</sub> storage material to absorb O<sub>2</sub> while oxygen of the exhaust gas is in high concentration and release the absorbed O<sub>2</sub> while oxygen is in low concentration, a NO<sub>x</sub> sensor disposed in the exhaust gas passage downstream of the NO<sub>x</sub> trap catalyst, an O<sub>2</sub> sensor disposed in the exhaust gas passage downstream of the NO<sub>x</sub> trap catalyst, an engine speed sensor operative to detect an engine speed, an accelerator opening sensor operative to detect an opening of an accelerator, an engine coolant temperature sensor operative to detect a temperature of an engine coolant, a control unit operative to receive output values of the respective sensors, and to control a fuel injector and an ignition timing of the engine and execute a diagnosis of deterioration of the NO<sub>x</sub> trap catalyst according to the received output values of the sensors, wherein the control unit calculates the amount of NO<sub>x</sub> absorbed in the NO<sub>x</sub> trap catalyst according to an output value of the NO<sub>x</sub> sensor, controls the fuel injector so as to lower the concentration of oxygen of the exhaust gas in the exhaust gas passage and thereby to cause the NO<sub>x</sub> trap catalyst to release NO<sub>x</sub> absorbed when the amount of the NO<sub>x</sub> absorbed in the NO<sub>x</sub> trap catalyst reaches a specified amount, determines that a specified diagnosis condition to diagnose the NO<sub>x</sub> trap catalyst is satisfied when the engine is warmed up with the engine coolant temperature that is greater than a specified temperature and the engine is in an ordinary state with a changing rate of the accelerator opening that is lower than a specified rate, detects whether or not O<sub>2</sub> release from the O<sub>2</sub> storage material caused by

oxygen concentration lowering of the exhaust gas in the exhaust gas passage has terminated according to the output value of the O<sub>2</sub> sensor, diagnoses, when the specified diagnosis condition is satisfied, that O<sub>2</sub> storage capacity of the O<sub>2</sub> storage material included in the NO<sub>x</sub> trap catalyst has deteriorated according to output values of the NO<sub>x</sub> sensor that are generated during a term from the beginning of the oxygen concentration lowering until a termination of the O<sub>2</sub> release from the O<sub>2</sub> storage material and that NO<sub>x</sub> reduction capacity of the catalytic metal included in the NO<sub>x</sub> trap catalyst has deteriorated according to an output value of the NO<sub>x</sub> sensor that is generated after a termination of the O<sub>2</sub> release from the O<sub>2</sub> storage material, and controls the fuel injector such that a speed of lowering oxygen concentration when the specified diagnosis condition is satisfied is slower than that when the specified diagnosis condition is not satisfied.

[0031] The seventeenth aspect of the present invention provides an exhaust gas purifying device of an engine, comprising a NO<sub>x</sub> trap catalyst disposed in an exhaust gas passage of the engine including a NO<sub>x</sub> trap material to absorb NO<sub>x</sub> while oxygen of an exhaust gas is in high concentration and release the absorbed NO<sub>x</sub> while oxygen is in low concentration, a catalytic metal to purify the NO<sub>x</sub> released from the NO<sub>x</sub> trap material, and an O<sub>2</sub> storage material to absorb O<sub>2</sub> while oxygen of the exhaust gas is in high concentration and release the absorbed O<sub>2</sub> while oxygen is in low concentration, a NO<sub>x</sub> sensor disposed in the exhaust gas passage downstream of the NO<sub>x</sub> trap catalyst, an O<sub>2</sub> sensor disposed in the exhaust gas passage downstream of the NO<sub>x</sub> trap catalyst, an engine speed sensor operative to detect an engine speed, an accelerator opening sensor operative to detect an opening of an accelerator, an engine coolant temperature sensor operative to detect a temperature of an engine coolant, a control unit operative to receive output values of the respective sensors, and to control a fuel injector and an ignition timing of the engine and execute a diagnosis of deterioration of the NO<sub>x</sub> trap catalyst, according to the received output values of the sensors, wherein the control unit calculates the amount of NO<sub>x</sub> absorbed in the NO<sub>x</sub> trap catalyst according to an output value of the NO<sub>x</sub> sensor, controls the fuel injector so as to lower the

concentration of oxygen of the exhaust gas in the exhaust gas passage and thereby to cause the NOx trap catalyst to release NOx absorbed when the amount of the NOx absorbed in the NOx trap catalyst reaches a specified amount, determines that a specified diagnosis condition to diagnose the NOx trap catalyst is satisfied when the engine is warmed up with the engine coolant temperature that is greater than a specified temperature and the engine is in an ordinary state with a changing rate of the accelerator opening that is lower than a specified rate, detects whether or not O<sub>2</sub> release from the O<sub>2</sub> storage material caused by oxygen concentration lowering of the exhaust gas in the exhaust gas passage has terminated according to the output value of the O<sub>2</sub> sensor, diagnoses, when the specified diagnosis condition is satisfied, that O<sub>2</sub> storage capacity of the O<sub>2</sub> storage material included in the NOx trap catalyst has deteriorated when an integrated value of output values of the NOx sensor with respect to time during a term from the beginning of the oxygen concentration lowering until a termination of the O<sub>2</sub> release from the O<sub>2</sub> storage material is smaller than a first threshold value and that NOx reduction capacity of the catalytic metal included in the NOx trap catalyst has deteriorated when a maximum value of output values of the NOx sensor that are generated after a termination of the O<sub>2</sub> release from the O<sub>2</sub> storage material is greater than a second threshold value, and controls the fuel injector such that a speed of lowering oxygen concentration when the specified diagnosis condition is satisfied is slower than that when the specified diagnosis condition is not satisfied.

#### BRIEF DESCRIPTION OF THE DRAWINGS

[0032] Other features, aspects, and advantages of the present invention will become apparent from the following description of the present invention which refers to the accompanying drawings.

[0033] FIG. 1 is a diagram showing a schematic structure of an engine system equipped with an exhaust gas purifying device according to a preferred embodiment of the present

invention.

[0034] FIG. 2 is a flowchart illustrating a sequence routine of an engine control executed by an ECU.

[0035] FIGS. 3A, 3B, and 3C are time charts illustrating respectively an air-fuel ratio, concentration of oxygen of an exhaust gas, and an output value of a NOx sensor 26, before and after a tailing control and a successive rich maintaining control.

[0036] FIG. 4 is a flowchart illustrating a sequence routine of a diagnosis control of deterioration of a NOx trap catalyst executed by the ECU.

#### DETAILED DESCRIPTION OF THE INVENTION

[0037] Hereinafter, preferred embodiments of the present invention will be described with reference to the accompanying drawings. FIG. 1 is a diagram showing a schematic structure of an engine system 100 of a spark-ignition engine equipped with an exhaust purifying device according to a preferred embodiment of the present invention.

[0038] The engine system 100 comprises an engine body 1. The engine system performs a lean burn operation in which an air-fuel ratio is set to a value leaner than 14.7 (stoichiometric air-fuel ratio) in a specified operating condition. The engine body 1 is equipped with a plurality of cylinders 2 (only one cylinder shown in the figure) and a piston 3 that is disposed in each cylinder 2 so as to reciprocate in the cylinder 2, defining a combustion chamber 4 with the cylinder 2 and the piston 3. The combustion chamber 4 is provided with an ignition plug 6 coupled to an ignition circuit 5 at the top of the combustion chamber 4 in such a manner that the ignition plug 6 faces the combustion chamber 4. Further, an injector 7 is provided to spray a fuel directly into the combustion chamber 4.

[0039] The injector 7 is coupled with a fuel supply circuit including a high-pressure fuel pump, a pressure regulator and the like. The fuel supply circuit regulates a fuel from a fuel tank at an appropriate pressure and the fuel is supplied to the injector 7. A fuel pressure

sensor 8 to detect a fuel pressure is provided in the fuel supply circuit.

[0040] The combustion chamber 4 communicates with an intake passage 10 through an intake port having an intake valve 9 therein. The intake passage 10 is provided, in order from an upstream end, with an air cleaner 11 to filter an intake air, an airflow sensor 12 to detect the amount of airflow, an electric-controlled throttle valve 13 to control a passage area of the intake passage 10, and a surge tank 14. The electric-controlled throttle valve 13 is driven by a motor 15 so as to open and close. Further, a throttle opening sensor 16 to detect a opening degree of the throttle valve 13 is disposed near the electric-controlled throttle valve 13, and an intake-air pressure sensor 17 to detect an intake air pressure is provided in the surge tank 14.

[0041] The intake passage 10 is comprised of independent passages branching off downstream of the surge tank 14, leading to respective cylinders. A downstream end of each independent passage is divided into two portions that lead to respective intake ports of an identical cylinder. A swirl valve 18 is disposed in either one of the divided portions. The swirl valve 18 is driven by an actuator 19. When the swirl valve 18 is closed, the intake air is supplied to the combustion chamber 14 only through the other branched passage, thereby generating a strong swirl of intake air in the combustion chamber 4. A swirl valve opening sensor 20 to detect an opening degree of the swirl valve 18 is also provided near the swirl valve 18.

[0042] The combustion chamber 4 is connected to an exhaust passage 22 through an exhaust port in which an exhaust valve 21 is disposed. The exhaust passages 22 from respective cylinders are merged downstream thereof. The merged exhaust passage 22 is provided, in order from an upstream end, with an upstream-side oxygen concentration sensor (O<sub>2</sub> sensor) 24a, a NO<sub>x</sub> trap catalyst 25, a downstream-side oxygen concentration sensor (O<sub>2</sub> sensor) 24b and a NO<sub>x</sub> sensor 26. The NO<sub>x</sub> trap catalyst 25 is of a NO<sub>x</sub> absorbing-and-reducing type that includes a NO<sub>x</sub> trap material and a catalytic metal (noble metal). The NO<sub>x</sub> trap material absorbs NO<sub>x</sub> while oxygen of an exhaust gas is in high

concentration, such as in a lean burn operation, and release the absorbed NO<sub>x</sub> while oxygen is in low concentration. The catalytic metal (noble metal) reduces and thereby purifies the NO<sub>x</sub> released from the NO<sub>x</sub> trap material.

[0043] The NO<sub>x</sub> trap catalyst 25 includes a carrier in honeycomb structure made of cordierite. An inner catalyst layer is coated on a wall surface of each through hole formed in the carrier, and an outer catalyst layer is coated on the inner catalyst layer.

[0044] In the inner catalyst layer having NO<sub>x</sub> absorbing catalytic function, a noble metal such as platinum and a NO<sub>x</sub> trap material such as barium are carried on a support material formed out of a porous material such as alumina or ceria. Meanwhile, in the outer catalyst layer having NO<sub>x</sub> reduction function, a catalytic metal such as platinum and rhodium and, if necessary, a NO<sub>x</sub> trap material such as barium are carried on a support material formed out of a porous material such as zeolite.

[0045] The NO<sub>x</sub> trap catalyst 25, which is also required to function as a three-way catalyst, includes an O<sub>2</sub> storage material such as ceria operative to store oxygen (O<sub>2</sub>) while the air-fuel ratio is lean and release stored O<sub>2</sub> while the air-fuel ratio is rich, thereby purifying HC and CO. Further, the O<sub>2</sub> storage material such as ceria also performs the function of causing the NO<sub>x</sub> trap material to improve its NO<sub>x</sub> absorption while the air-fuel ratio is lean.

[0046] Because the NO<sub>x</sub> trap catalyst 25 is limited in its NO<sub>x</sub> absorbing capacity, the present embodiment is configured such that when NO<sub>x</sub> value of the exhaust gas detected by the NO<sub>x</sub> sensor 26 exceeds a specified value equivalent to a value with some margin to the limited amount of NO<sub>x</sub> absorption (smaller than the limited amount), the amount of absorbed NO<sub>x</sub> by NO<sub>x</sub> trap material included in the NO<sub>x</sub> trap catalyst is determined to have reached a region where NO<sub>x</sub> purge is needed (saturation or near saturation), and then a control (rich-spike control) for releasing NO<sub>x</sub> from the NO<sub>x</sub> trap material is executed by lowering the oxygen concentration of the exhaust gas.

[0047] There is provided an exhaust gas recirculation passage 27 for recirculating part of the exhaust gas to an intake system, an upper-stream end of which is connected to the

exhaust passage 22 upstream of the upstream-side oxygen concentration sensor 24a. A down-stream end of the exhaust gas recirculation passage 27 is connected with the intake passage 10 between the throttle valve 13 and the surge tank 14. Further, the exhaust gas recirculation passage 27 is provided with an exhaust gas recirculation valve 28 being electrically adjustable in its opening degree and a lift sensor 29 to detect the amount of lift of the exhaust gas recirculation valve 28. These components constitute exhaust gas recirculation means.

[0048] Further, there is provided a secondary-air supply passage 30 which supplies part of intake air from the intake passage 10 to the exhaust passage 22 upstream of the NOx trap catalyst 25. A flow regulating valve 31 is adjustably provided in the secondary-air supply passage 30.

[0049] The engine system 100 further comprises an ECU (electric control unit) 32 to control an entire system. Various signals of the airflow sensor 12, the throttle opening sensor 16, the intake-air pressure sensor 17, the swirl-valve opening sensor 20, the upstream-side and downstream-side oxygen concentration sensor 24a, 24b, and the lift sensor 29 of the exhaust gas recirculation valve 28 are inputted to the ECU 32. The ECU 32 further receives output signals of an engine coolant temperature sensor 33 to detect a temperature of coolant of the engine 1, an intake-air temperature sensor 34 to detect a temperature of intake air, an atmospheric pressure sensor 35 to detect a pressure of the atmosphere, engine speed sensor 36 to detect an engine speed, an accelerator opening sensor 37 to detect an opening degree of an accelerator pedal (operating amount of accelerator pedal), and the like.

[0050] The ECU 32 executes, according to the engine operating condition, a fuel injection control operative to control a fuel injection state of fuel injected by the injector 7, an ignition timing control operative to control an ignition timing of a mixture air by the ignition plug 6, a rich-spike control operative to release NOx from the NOx trap catalyst 25 by controlling the oxygen concentration of the exhaust gas when the amount of NOx

absorbed at the NOx trap catalyst 25 reaches a specified amount, and deterioration diagnosing control operative to diagnose a degree of deterioration of the NOx trap catalyst 25 along with the rich-spike control and the like under a specified condition.

[0051] The fuel injection control is configured such that the fuel injection is controlled according to the engine operating condition. In the present embodiment, a stratified combustion mode control is performed in a lean operation region allotted for a driving condition with low speed and low load through moderate speed and moderate load, in which the injector 7 sprays fuel at one time at a specified timing during a compression stroke of the engine so as to concentrate sprayed fuel locally around the ignition plug 6, with the mixture being in a lean state of the air-fuel ratio of about 30. Meanwhile, in a first rich operation region allotted for a driving condition with a higher load than the stratified combustion mode, a stoichiometric combustion mode is performed in which the injector 7 sprays fuel at two times during an intake stroke and a compression stroke of the engine, with the mixture being in a stoichiometric state of  $\lambda=1$ . Further, in a second rich operation region allotted for a driving condition with higher speed and higher load than the first rich operation region, a homogeneous combustion mode is performed in which the injector 7 sprays fuel at one time during an intake stroke of the engine, with the mixture being in a rich state in the combustion chamber 4.

[0052] NOx generated in a large amount in the lean-burn state, is absorbed by the NOx trap catalyst 25 disposed downstream. In the present embodiment, the amount of NOx absorbed in the NOx trap catalyst 25 is estimated according to the output signal of the NOx sensor 26. When it is determined that NOx absorption of the NOx trap catalyst 25 has saturated, a control such as air-fuel ratio control (rich-spike control) is executed to lower the oxygen concentration of the exhaust gas, for example, to 0.3% or less, thereby causing the NOx trap catalyst 25 to release the absorbed NOx. Further, the deterioration diagnosis of the NOx trap catalyst 25 is also executed according to the output signal of the NOx sensor 26 at this time. In the present embodiment, there is provided indication means 41,

including a warning lamp and the like, that notifies a driver of the deterioration when it is determined that the NOx trap catalyst **25** has deteriorated.

[0053] Next, engine control process performed by the ECU **32** will be described referring to the flowchart of FIG. 2. In the present embodiment, when the amount of absorbed NOx has reached the saturation amount or an amount close to this, the rich-spike control is performed by changing the air-fuel ratio to lower the oxygen concentration of the exhaust gas, thereby causing the NOx trap catalyst to release NOx therefrom. Further, in the present embodiment, a speed or rate at which the oxygen concentration is lowered in the rich-spike control is controlled to be slower when the deterioration diagnosis of the NOx trap catalyst is executed along with the rich-spike control.

[0054] Firstly, in step S1, output signals of the airflow sensor **12**, the upstream-side oxygen concentration sensor **24a**, the NOx sensor **26**, the engine coolant temperature sensor **33**, the intake-air temperature sensor **34**, the atmospheric pressure sensor **35**, the engine speed sensor **36**, the accelerator opening sensor **37** and the like are inputted as data. Next, in step S2, a basic fuel injection amount  $Q_b$ , a basic fuel injection timing  $I_b$ , and an ignition timing  $\theta_b$  are set according to the data inputted in step S1. Next, the sequence proceeds to step S3 where a basic throttle valve opening  $T_{vb}$  is set according to the data inputted in step S1.

[0055] Next, the sequence proceeds to step S4 where NOx absorbed amount NOes in the NOx trap catalyst **25** is estimated according to the output of the NOx sensor **26**, and in step S5, it is determined whether the NOes is greater than a specified threshold value NOeso or not. The threshold value NOeso is a value to be used in the determination as to whether or not the amount of absorbed NOx of the NOx trap catalyst **25** has reached the saturation amount or an amount close to this. When the answer to step S5 is Yes, the NOx trap catalyst **25** has absorbed NOx up to its saturation value, meaning that the rich-spike control for releasing NOx is needed.

[0056] When the answer to step S5 is YES, the sequence proceeds to step S6 where it is

determined whether or not a condition for executing the deterioration diagnosis (monitor) of the NOx trap catalyst 25 is satisfied. Namely, it is determined whether or not the operating condition is in a lean operation, an ordinary operation state, a warmed-up state and the number of times of the deterioration diagnosis held after an ignition ON is less than two times. When the answers to these are all YES, it is considered that the monitor condition has been satisfied. Herein, the “ordinary operation state” is an additional condition for the deterioration diagnosis so that the diagnosis can be performed accurately. The ordinary operation state is determined, for example, when a vehicle acceleration is less than a specified value, or the accelerator opening is less than a specified value. Also, “warmed-up state” is an another additional condition for executing the deterioration diagnosis of the NOx trap catalyst in a specified warmed-up state in which the NOx trap catalyst is in an activated state. The warm-up state is determined, for example, when the intake-air temperature or the engine coolant temperature is greater than a specified temperature or a specified time has passed since an engine starts. Herein, the number of times of the deterioration diagnosis described above may be set to one or less.

[0057] When the answer to step S6 is NO, namely when the monitor condition is not satisfied, a normal rich-spike control without the deterioration diagnosis is performed. Namely, the sequence proceeds to step S7, and 1 is added to a timer  $T\lambda$  (increment) for rich-spike control. Then, in step S8, it is determined whether or not a value of the timer  $T\lambda$  exceeds a specified value  $T\lambda_0$ . When the answer to step S8 is NO, the sequence proceeds to step S9 where a throttle valve opening  $Tv$  is set to a throttle valve opening  $Tv\lambda$  for rich-spike control. Then, in step S10, the throttle valve is driven so as to open at the throttle valve opening  $Tv\lambda$ . In the rich-spike control, the throttle valve opening  $Tv\lambda$  for the rich-spike control is smaller than the throttle valve opening in a lean burn state so that the combustion is executed in the rich state and the oxygen concentration of the exhaust gas is lowered.

[0058] Subsequently, in step S11, the fuel injection amount, fuel injection timing and

ignition timing are set respectively to a fuel injection amount  $Q\lambda$ , a fuel injection timing  $I\lambda$  and an ignition timing  $\theta\lambda$  for the rich-spike control. In the present embodiment, a split injection is performed during the rich-spike control operation, in which fuel injection is split into two-time injections and each of them is performed during the intake stroke and the compression stroke, respectively. Accordingly, the amount of fuel injection is set as an injection amount for the intake stroke and an injection amount for the compression stroke, respectively. Also, the timing of fuel injection is set as an injection timing for the intake stroke and an injection timing for the compression stroke. Herein, the injection amount, in the present embodiment, is set to an amount equivalent to an air-fuel ratio which is less than 14.5, so that the oxygen concentration of the exhaust gas is less than 0.3%. Accordingly, after the control begins, the oxygen concentration of the exhaust gas rapidly lowers to rich air-fuel ratio, for example, within one second.

[0059] When the answer to step S8 is YES,  $T\lambda$  is reset in step S12 and then NOes is reset in step S13 so as to terminate the rich-spike control because the specified time has passed.

[0060] When the answer to step S6 is YES, the sequence proceeds to step S14 so as to execute the deterioration diagnosis of the NOx trap catalyst **25** along with the rich-spike control. In the present embodiment, at first tailing control for gradually lowering the oxygen concentration of the exhaust gas is performed in the rich-spike control which is performed along with the deterioration diagnosis of the NOx trap catalyst **25**.

[0061] In step S14, it is determined whether an actual air-fuel ratio A/F reaches a final target air-fuel ratio  $A/F\lambda$  or not. The final target air-fuel ratio is set such that it is a stoichiometric air-fuel ratio  $\lambda=1$  before it is determined that O<sub>2</sub> storage capacity of the NOx trap catalyst has deteriorated, while it is slightly leaner air-fuel ratio than  $\lambda=1$  ( $A/F=15-16$ ) when it is determined that O<sub>2</sub> storage capacity of the NOx trap catalyst has deteriorated. The determination in step S14 is executed, for example, according to the output of the upstream-side oxygen concentration sensor **24a**. When the answer to step S14 is YES, a target air-fuel ratio  $A/F_{ref}$  is decreased by  $\alpha$  in step S15. It is preferable that a value of  $\alpha$

should be set to a value with which the air-fuel ratio changes from a lean state having a value greater than 22 to the stoichiometric air-fuel ratio state having a value of 14.7 in, for example, 5 seconds or so.

[0062] Next, the throttle valve opening  $T_v$  is set based on the decreased target air-fuel ratio A/Fref in step S16, and the throttle valve is driven according to this opening in step S17.

[0063] Subsequently, in step S18, a fuel injection amount  $Q_{mc}$ , a fuel injection timing  $I_{mc}$  and an ignition timing  $\theta_{mc}$  for the tailing control are set respectively based on the target air-fuel ratio A/Fref set in step S15. Then, a flag  $F_{mc}$  for indicating is set to 1 in step S19.

[0064] Meanwhile, when the answer to step S14 is NO, namely when the actual air-fuel ratio is equal to the final target air-fuel ratio, a process for maintaining a rich (final target air-fuel) state is performed for a specified time. That is, the sequence proceeds to step S20 for resetting the flag  $F_{mc}$ , and then to step S21 for adding 1 to the timer  $T_m$ , which is used for maintaining the rich state, for timer increment, and subsequently to step S22 for determining whether the value of timer  $T_m$  exceeds a specified value  $T_{m0}$  or not. When the answer to step S22 is NO, the sequence proceeds to step S23 for setting the throttle valve opening  $T_v$  to a throttle valve opening  $T_{v\lambda2}$  for a rich air-fuel ratio (final target air-fuel ratio), and then in step S24, the throttle valve is adjusted so as to open at the throttle valve opening  $T_{v\lambda2}$ . Next, in step S25, the fuel injection amount, fuel injection timing and ignition timing are set respectively to a fuel injection amount  $Q_{\lambda2}$ , a fuel injection timing  $I_{\lambda2}$  and an ignition timing  $\theta_{\lambda2}$  for maintaining the rich (final target air-fuel ratio).

[0065] Meanwhile, when the answer to step S22 is YES, this means that the time period, during which the rich (target air-fuel ratio) state is maintained, has passed. Accordingly, the sequence proceeds to step S26 for resetting  $T_m$  and then to step S27 for resetting NOes.

[0066] When the answer to step S5 is NO, the sequence proceeds to step S28 where it is determined whether counting  $T_{\lambda}$  is in process or not. When the answer to step S28 is YES, meaning that the rich-spike control is in process, the sequence proceeds to step S7. When

the answer to step S28 is NO, the sequence proceeds to step S29 for determining whether the flag Fmc for the tailing control is 1 or not. When the answer to S29 is YES, meaning that the tailing control is in process, the sequence proceeds to step S14. When the answer to step S29 is NO, the sequence proceeds to step S30 for determining whether or not counting the timer Tm indicating the duration of maintaining the rich (final target air-fuel ratio) state is in process. When the answer to step S30 is YES, the sequence proceeds to step S21. After step S11, step S13, step S19, step S25, step S27 and step S30 are terminated, the sequence proceeds to step S31 for executing the fuel injection in the set injection amount and timing, and then to step S32 for executing the ignition at the set timing.

[0067] FIGS. 3A, 3B, and 3C are time charts illustrating respectively the air-fuel ratio, concentration of oxygen of the exhaust gas, and output of the NOx sensor 26, before and after the tailing control and the successive rich (final target air-fuel ratio) maintaining control, which are performed for the deterioration diagnosis of the NOx trap catalyst 25 in the present embodiment.

[0068] The air-fuel ratio of the exhaust gas is in a lean state just before the beginning of NOx release from the NOx trap catalyst 25. In the present embodiment, the air-fuel ratio control is performed in such a manner that it takes approximately five seconds to change from this lean state (for example, the air-fuel ratio of 22 or more) to a state with the air-fuel ratio of  $\lambda=1$ . Namely, the time from t1 to t3 in FIGS. 3A through 3C is set so as to be approximately five seconds. In the present embodiment, when it is recognized based on the output of the upstream-side oxygen concentration sensor 24a that the oxygen concentration of the exhaust gas upstream of the NOx trap catalyst 25 drops to the oxygen concentration of 0.5% which is equivalent to the air-fuel ratio of 14.7 (the final target air-fuel ratio), the tailing control is terminated and the air-fuel ratio is maintained at this state.

[0069] When this rich-spike control begins (at t1), the oxygen concentration (the

upstream-side oxygen concentration) of the exhaust gas flowing into the NO<sub>x</sub> trap catalyst 25 lowers due to the lowering of the air-fuel ratio, and O<sub>2</sub> release from the O<sub>2</sub> storage material included in the NO<sub>x</sub> trap catalyst 25 is executed (FIG. 3B). Accordingly, during the O<sub>2</sub> release from the O<sub>2</sub> storage material, the oxygen concentration of the exhaust gas surrounding the NO<sub>x</sub> trap catalyst shifts toward a leaner side (namely, to leaner air-fuel ratio) and thereby NO release from the NO<sub>x</sub> trap material is suppressed. Thus, when O<sub>2</sub> release from the O<sub>2</sub> storage material has terminated, the lean-shifting of the exhaust gas surrounding the NO<sub>x</sub> trap catalyst disappears, so that NO<sub>x</sub> release from the NO<sub>x</sub> trap material increases rapidly. Herein, when O<sub>2</sub> release from the O<sub>2</sub> storage material has terminated (at t<sub>2</sub>), the O<sub>2</sub> concentration of the exhaust gas downstream of the NO<sub>x</sub> trap catalyst 25 lowers rapidly, and thus, completion of O<sub>2</sub> release from the O<sub>2</sub> storage material can be detected according to the O<sub>2</sub> concentration of the exhaust gas downstream of the NO<sub>x</sub> trap catalyst.

[0070] Accordingly, when the air-fuel ratio lowers, the amount of NO<sub>x</sub> release from the NO<sub>x</sub> trap material included in the NO<sub>x</sub> trap catalyst 25 increases gradually from NO<sub>in</sub>. The amount of this NO<sub>x</sub> release increases rapidly when the O<sub>2</sub> release from the O<sub>2</sub> storage material has terminated (at t<sub>2</sub>), and increases up to a peak value (NO<sub>max</sub>), and then it drops to NO<sub>min</sub> (at t<sub>4</sub>) and maintains its approximately constant level after that. In the present embodiment, as described above, a state of NO<sub>x</sub> release of the NO<sub>x</sub> trap catalyst when the air-fuel ratio is lowered for reducing the oxygen concentration is divided into two stages (t<sub>1</sub> – t<sub>2</sub>, t<sub>2</sub> – t<sub>4</sub>). Herein, output values (the region indicated by mesh in FIG. 3C) of the NO<sub>x</sub> sensor at a first stage (t<sub>1</sub> – t<sub>2</sub>) relates to a degree of deterioration of the O<sub>2</sub> storage capacity of the O<sub>2</sub> storage material included in the NO<sub>x</sub> trap catalyst (the deterioration of the O<sub>2</sub> storage material), while output values (the region indicated by oblique lines in FIG. 3C) of the NO<sub>x</sub> sensor at a second stage (t<sub>2</sub> – t<sub>4</sub>) relates to a degree of deterioration of the NO<sub>x</sub> reduction capacity of the catalytic metal included in the NO<sub>x</sub> trap catalyst (the deterioration of the catalytic metal). Thus, the degree of deterioration of the O<sub>2</sub> storage capacity of the

O<sub>2</sub> storage material included in the NO<sub>x</sub> trap catalyst (the deterioration of the O<sub>2</sub> storage material), and the degree of deterioration of the NO<sub>x</sub> reduction capacity of the catalytic metal included in the NO<sub>x</sub> trap catalyst (the deterioration of the catalytic metal) can be diagnosed according to the output values of the NO<sub>x</sub> sensor at each of these stages.

[0071] Next, deterioration diagnosis process of the NO<sub>x</sub> trap catalyst **25**, which is executed by the ECU **32**, will be described referring to the flowchart of FIG. 4.

[0072] Firstly, in step S40, data of accelerator opening, accelerator opening change, engine speed, engine coolant temperature and the like are inputted. Next, the sequence proceeds to step S41 where the same determination as step S6 of FIG. 2 is made, namely the determination is made as to whether a condition for starting a monitor (diagnosis) is satisfied or not. When the answer to S41 is YES, the sequence proceeds to step S42 for calculating the amount of absorbed NO<sub>x</sub> in the NO<sub>x</sub> trap catalyst **25** according to the output value of the NO<sub>x</sub> sensor **26** and the engine operating conditions. Namely, because the amount of NO<sub>x</sub> of the exhaust gas upstream of the NO<sub>x</sub> trap catalyst **25** can be estimated according to the engine operating conditions and the amount of NO<sub>x</sub> in the exhaust gas downstream of the NO<sub>x</sub> trap catalyst **25** can be estimated according to the output of the NO<sub>x</sub> sensor **26**, the amount of absorbed NO<sub>x</sub> of the NO<sub>x</sub> trap catalyst **25** can be calculated based on a look-up table storing some reference values that have been obtained through experiments in advance.

[0073] Subsequently, the sequence proceeds to step S43, and herein a process for correcting the threshold value for the deterioration of O<sub>2</sub> storage material and the threshold value for the deterioration of catalytic material is executed according to the absorbed NO<sub>x</sub> amount of the NO<sub>x</sub> trap catalyst **25** that has been calculated in step S42. Specifically, the process is executed in such a manner that the greater the difference between the absorbed NO<sub>x</sub> amount calculated in step S42 and the threshold value for starting rich-spike control NO<sub>eso</sub> (the specified value) is, the greater value a first threshold value for diagnosing the deterioration of O<sub>2</sub> storage capacity of the NO<sub>x</sub> trap catalyst **25**, which will be described

later, is corrected to. Thus, the determination of deterioration of the O<sub>2</sub> storage material becomes apt to occur. Further, the process is executed in such a manner that the greater the difference between the absorbed NO<sub>x</sub> amount calculated in step S42 and the threshold value for starting rich-spike control NO<sub>es0</sub> (the specified value) is, the smaller value a second threshold value for diagnosing the deterioration of O<sub>2</sub> storage capacity of the NO<sub>x</sub> trap catalyst 25 which will be described later is corrected to. Thus, the determination of deterioration of the O<sub>2</sub> storage material becomes apt to occur.

[0074] In the event that extremely larger amount of NO<sub>x</sub> than the specified amount has been absorbed in the NO<sub>x</sub> trap catalyst, because of the engine's shut-down during the previous rich-spike control or other reasons, deterioration diagnosis of the O<sub>2</sub> storage material by using the normal threshold value would lead to the erroneous diagnosis result that the O<sub>2</sub> storage material has not yet deteriorated due to the large amount of absorbed NO<sub>x</sub>, in spite of the fact that it has already deteriorated. For this reason, when it is determined that the amount of NO<sub>x</sub> absorbed in the NO<sub>x</sub> trap catalyst is greater than the specified amount which is the threshold value for determining the start of the rich-spike control, the threshold value for determining deterioration of O<sub>2</sub> storage capacity is corrected in such a manner that determination of the deterioration of O<sub>2</sub> storage capacity becomes apt to occur, according to the difference between the absorbed NO<sub>x</sub> amount and the specified value of the threshold value, thereby preventing such erroneous diagnosis.

[0075] Further, at least one of threshold values for deterioration diagnosis of the catalytic metal included in the NO<sub>x</sub> trap catalyst (third, fourth and fifth threshold values), which will be described later, is corrected in such a manner that the greater a difference between the amount of absorbed NO<sub>x</sub> calculated in step S42 and a threshold value for the start of rich-spike control (specified amount) is, the greater value the threshold values is corrected to. Thus, the determination of deterioration of the catalytic metal becomes unlikely to occur.

[0076] In the event that extremely larger amount of NO<sub>x</sub> than the specified amount has

been absorbed in the NOx trap catalyst, because of the engine's shut-down during the previous rich-spike control or other reasons, deterioration diagnosis of the catalytic metal by using the normal threshold value would lead to erroneous diagnosis result that the catalytic metal has not deteriorated due to the large amount of absorbed NOx in spite of the fact that it has already deteriorated. For this reason, when it is determined that the amount of NOx absorbed in the NOx trap catalyst is greater than the specified amount which is the threshold value for determining the start of the rich-spike control, the threshold value for determining deterioration of catalytic metal storage is corrected in such a manner that determination of the deterioration of the catalytic metal becomes unlikely to occur, according to the difference between the absorbed NOx amount and the specified value of the threshold value, thereby preventing such erroneous diagnosis.

[0077] Further, a specified time to be used for diagnosing O2 storage capacity of the NOx trap catalyst, which will be described later, is corrected in such a manner that the greater a difference between the amount of absorbed NOx calculated in step S42 and a threshold value for the start of rich-spike control (specified amount) is, the longer value the specified time is corrected to. Thus, the determination of deterioration of the O2 storage capacity becomes apt to occur.

[0078] In the present embodiment, the first through fourth threshold values are corrected in step S43, and the specified time used for the deterioration diagnosis of the O2 storage capacity, which will be described later, is corrected. However, these may not be necessarily corrected, otherwise either one of these threshold values and specified time may be corrected.

[0079] When the process of step S43 terminates, the sequence proceeds to step S44 where it is determined whether or not the air-fuel ratio has just changed from  $\lambda=1$  (rich state) to lean state. This aims at determining whether the rich-spike control has just terminated or not.

[0080] Then the answer to step S44 is NO, the sequence proceeds to step S45 for

determining whether or not the air-fuel ratio has just started changing from lean state to  $\lambda=1$  (rich state) (that is, whether the time is after t1 or not). When the answer to step S45 is YES, the rich-spike control is in process, accompanied by the deterioration diagnosis. Accordingly, the sequence proceeds to step S46 for storing output values of the NOx sensor 26. Subsequently, the sequence proceeds to step S47 where it is determined whether or not the output value of the downstream-side oxygen concentration sensor 25b is lower than a value indicating the downstream-side oxygen concentration of the exhaust gas with the air-fuel ratio  $\lambda=1$ . When the answer to step S47 is NO, the current time point is within the term of  $t_1 - t_2$  when O<sub>2</sub> release from the O<sub>2</sub> storage material included in the NOx trap catalyst 25 continues. Accordingly, the sequence proceeds to step S46 where the process for storing the output of the NOx sensor 26 is repeated until the answer to step S47 turns to YES. An output of the NOx sensor 26 stored initially in step S46 is stored as NOin, while an output of the NOx sensor 26 stored finally in step S46 is stored as NOst.

[0081] When the answer to step S47 is YES, it is determined that t2 has been reached in FIG. 3C, and then the sequence proceeds to step S48 for calculating and storing the NOx output values NOin and NOst, the time ( $t_2 - t_1$ ) and an integration value (NO1) of the output value of the NOx sensor with respect to the term ( $t_1 - t_2$ ). Next, the sequence proceeds to step S49 for determining whether the output of the NOx sensor 26 is equal to NOin or not. When the answer to step S49 is NO, the current time point is within the term of t2 through t4. Accordingly, the sequence proceeds to step S50 for storing the output value of the NOx sensor 26, and the process of step S50 is repeated until the output value of the NOx trap sensor 26 turns to NOin.

[0082] When the answer to step S49 is YES, this instant is set as t4, and then the sequence proceeds to step S51. In step S51, the output value of the NOx sensor at this instant is stored as NOmin, and the maximum value NOmax of output values of the NOx sensor 26 during the term from t2 through t4 and an integrated value (NO2) of output values of the NOx sensor during the term ( $t_2 - t_4$ ) are calculated and stored, and the sequence returns.

[0083] On the other hand, when the answer to step S44 is YES, the sequence proceeds to step S52 for the increment of timer TL, and then to step S53 for determining whether the timer TL exceeds a specified value TLO or not. When the answer to step S44 is YES, the rich-spike control has terminated, and then a time for stabilization is kept in steps S52 and S53.

[0084] When the answer to step S53 is YES, the sequence proceeds to step S54 where it is determined whether or not the sum of the above integration values NO1 and NO2 is less than the threshold value for determining a degree of NOx absorption. When the answer to step S54 is YES, namely  $(NO1 + NO2)$  is less than the threshold value for determining degree of NOx absorption (sixth threshold value), it is determined that NOx trap capacity of the NOx trap material included in the NOx trap catalyst **25** has deteriorated (deterioration diagnosis). Accordingly, in step S55, the fact that NOx trap capacity of the NOx trap catalyst **25** has deteriorated is stored readably in a memory and executes warning such as tuning on a warning lamp or the like.

[0085] When the answer to step S54 is NO and the process of step S55 terminates, the sequence proceeds to step S56 for executing deterioration diagnosis of the O2 storage material included in the NOx trap catalyst **25**.

[0086] In the purification device of the present embodiment, at least one of the following three methods of deterioration diagnosis is or are executed. The first method is to determine that O2 storage capacity of the O2 storage material included in the NOx trap catalyst **25** has deteriorated when an integrated value of output values of the NOx sensor with respect to the time during the term from the beginning point (t1) of oxygen concentration lowering (rich-spike control) by the air-fuel ratio control until the terminating point (t2) of O2 release from the O2 storage material is less than a specified threshold value (first threshold value). The second method is to determine that O2 storage capacity of the O2 storage material included in the NOx trap catalyst **25** has deteriorated when a value that is gained by dividing a difference between the maximum value and the minimum value of

output values of the NOx sensor that are generated during the term from the beginning point (t1) of the rich-spike control by the air-fuel ratio control until the terminating point (t2) of O<sub>2</sub> release from the O<sub>2</sub> storage material, by the time of the term (t1 – t2) is greater than a specified threshold value(second threshold value). The third method is to determine that O<sub>2</sub> storage capacity of the O<sub>2</sub> storage material included in the NOx trap catalyst 25 has deteriorated when the time from the beginning point (t1) of the rich-spike control until the terminating point (t2) of O<sub>2</sub> release from the O<sub>2</sub> storage material is a specified time.

[0087] These threshold values and the specified time are corrected appropriately in step S43, according to the amount of NOx absorbed in the NOx trap catalyst.

[0088] When the deterioration diagnosis terminates, the sequence proceeds to step S57 where it is determined whether O<sub>2</sub> storage capacity has deteriorated or not, namely the O<sub>2</sub> storage material has deteriorated or not. In the present embodiment, when the plurality of methods of deterioration diagnosis are executed, at least one deterioration determination gives the diagnosis result that O<sub>2</sub> storage capacity has deteriorated (O<sub>2</sub> storage deterioration). When the answer to step S57 is YES, the sequence proceeds to step S58, and the fact that O<sub>2</sub> storage capacity of the O<sub>2</sub> storage material has deteriorated (deterioration of O<sub>2</sub> storage material) is stored readably in a memory and executes warning such as tuning on a warning lamp or the like.

[0089] Next, the sequence proceeds to step S59 for setting the target air-fuel ratio (A/F) at the rich-spike control to a value that is leaner than  $\lambda=1$ . Namely, in order to compensate for some amount of O<sub>2</sub> released from the O<sub>2</sub> storage material during the rich-spike control, oxygen concentration of the exhaust gas in the exhaust passage which is materialized by the air-fuel ratio control is set to a value lower than a value which is actually required in the exhaust passage. For this reason, if O<sub>2</sub> storage capacity of the O<sub>2</sub> storage material has deteriorated, an expected amount of O<sub>2</sub> may not be released from the O<sub>2</sub> storage material, so that the oxygen concentration of the exhaust gas in the exhaust passage at the rich-spike control may be less than the target value. Herein, in the present embodiment, when the

amount of O<sub>2</sub> released from the O<sub>2</sub> storage material included in the NO<sub>x</sub> trap catalyst is decreased at the rich-spike control due to the deterioration of O<sub>2</sub> storage capacity of the O<sub>2</sub> storage material, the oxygen concentration of the exhaust gas in the exhaust passage at the rich-spike control is set to a higher value than that when O<sub>2</sub> storage capacity of the O<sub>2</sub> storage material has not deteriorated yet in step S59. In this manner, enough oxygen concentration of the exhaust gas in the exhaust passage during the rich-spike control can be ensured even when O<sub>2</sub> storage capacity of the O<sub>2</sub> storage material has deteriorated.

[0090] When the answer to step S57 is NO or the process of step S59 terminates, the sequence proceeds to step S60 and deterioration diagnosis of the catalytic metal included in the NO<sub>x</sub> trap catalyst 25 is executed.

[0091] In the purifying device of the present invention, at least one of the flowing three methods of deterioration diagnosis is executed. The first method is to determine that NO<sub>x</sub> reduction capacity of the catalytic metal included in the NO<sub>x</sub> trap catalyst 25 has deteriorated when the maximum value (NOmax) of output values of the NO<sub>x</sub> sensor that are generated after the terminating point (t2) of O<sub>2</sub> release from the O<sub>2</sub> storage material is greater than a specified threshold value (third threshold value).

[0092] Further, the second method is to determine that NO<sub>x</sub> reduction capacity of the catalytic metal included in the NO<sub>x</sub> trap catalyst 25 has deteriorated when an integrated value of output values of the NO<sub>x</sub> sensor with respect to the time during the term from the terminating point (t2) of O<sub>2</sub> release from the O<sub>2</sub> storage material until a point (t4) when a specified time has passed since the terminating point of O<sub>2</sub> release is grater than a specified threshold value (fourth threshold value).

[0093] Further, the third method is to determine that NO<sub>x</sub> reduction capacity of the catalytic metal included in the NO<sub>x</sub> trap catalyst 25 has deteriorated when a value that is gained by dividing a difference between a maximum value NOmax of output values of the NO<sub>x</sub> sensor that are generated during a term from the terminating point (t2) of O<sub>2</sub> release from the O<sub>2</sub> storage material until the point (t4) when the specified time has passed since

the terminating point and an output value NOxin of the NOx sensor that is generated at the time when the O<sub>2</sub> release from the O<sub>2</sub> storage material has terminated, by a difference between the output value of the NOx sensor that is generated at the point (t2) when the O<sub>2</sub> release from the O<sub>2</sub> storage material has terminated and an output value of the NOx sensor that is generated at the point (t4) when the specified time has passed is greater than a specified value (fifth threshold value).

[0094] These threshold values are corrected appropriately in step S43 according to the amount of NOx absorbed in the NOx trap catalyst.

[0095] When deterioration diagnosis of the catalytic metal terminates, the sequence proceeds to step S61 for determining whether reduction capacity of the catalytic metal has lowered or not, namely the catalytic metal has deteriorated or not. In the present embodiment, when the plurality of methods of deterioration diagnosis are executed, at least one deterioration determination gives the diagnosis result that NOx reduction capacity has deteriorated (catalytic metal deterioration). When the answer to step S61 is YES, the sequence proceeds to step S62, and the fact that NOx reduction capacity of the catalytic metal has deteriorated (deterioration of catalytic metal) is stored readably in a memory and executes warning such as tuning on a warning lamp or the like.

[0096] Next, the sequence proceeds to step S63 where the threshold value NOeso for starting the rich-spike control is corrected to a smaller value. Because NOx reduction capacity of the catalytic metal included in the NOx trap catalyst has deteriorated and thereby the mount of NOx which can be reduced by the catalytic metal has lowered, the rich-spike control is performed under a condition that the amount of NOx absorbed in the NOx trap catalyst is small. Accordingly, NOx can be prevented from being emitted out of the engine exhaust system. When the answer to step S61 is NO or process in step S63 has terminated, the sequence returns.

[0097] Further, when the answer to S41 is NO, the sequence proceeds to step S64. In this step, data such as output values of the NOx sensor, output values of the oxygen

concentration sensor, timer TL, NOst, NOin, NOmin, NOmax, time pasting of (t1 – t2), output-integrated value (NO1) of the NOx sensor from t1 until t2, output-integrated value (NO2) of the NOx sensor from t2 until t4 and the like are reset, and then the sequence returns. When the answer to step S43 is NO, the sequence returns as well.

[0098] Any other additional modifications may be applied within the scope of a spirit of the present invention.

[0099] For example, in the above-described embodiment, it is determined according to the output of the upstream-side oxygen concentration sensor 24a in step S14 whether or not the actual air-fuel ratio A/F reaches a value A/F $\lambda$  which is air-fuel ratio  $\lambda=1$ . Instead of this, the determination may be made when a specified time has passed since the beginning point of the tailing control. Further, other methods of diagnosing the deterioration may be applied as well.

[00100] Further, the present embodiment shows an example in which the air-fuel ratio is controlled so as to change from a lean state to a state with  $\lambda=1$  for five seconds or so. Of course, the present invention should not be limited by the exemplified time, and a proper time can be chosen, for example, from a range of three seconds through thirty seconds, based on various conditions.